Targets for Heavy Ion Fusion Energy

L. John Perkins Lawrence Livermore National Laboratory

With contributions from: B.G.Logan², E.Henestroza², J.Barnard¹, A.Friedman¹, M.Terry¹, D.Callahan¹, M.Tabak¹, P.Seidl², M.Hay³, D.Bailey¹

1.Lawrence Livermore National Laboratory, 2.Lawrence Berkeley National Laboratory, 3.Princeton Plasma Physics Laboratory

The National Academies Panel on Assessment of Inertial Confinement Fusion Targets,
Washington, DC
February 16, 2011

This work was performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under Contract DE-AC52-07NA27344. Lawrence Livermore National Laboratory, P.O. Box 808, Livermore, CA 94551









Heavy ion fusion: Induction accelerator drivers are durable, efficient, and enable high pulse rates (like transformers)





Heavy ion accelerators of multi-MJ fusion scale would be comparable in scale to today's large NP accelerators like GSI-FAIR, RHIC \Rightarrow Economical for 1-2 GW_e baseload power plants.

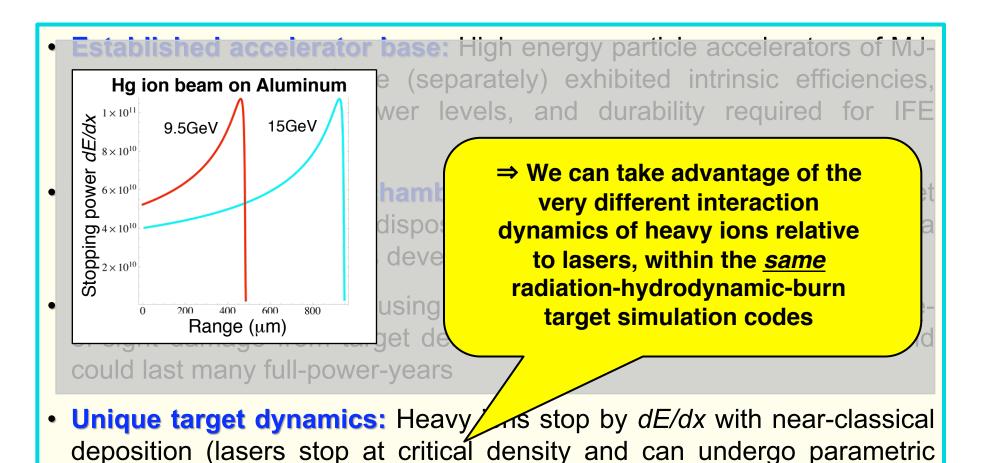
Why heavy-ion drivers for inertial fusion energy?



- Established accelerator base: High energy particle accelerators of MJ-scale beam kinetic energy have (separately) exhibited intrinsic efficiencies, pulse-rates, average power levels, and durability required for IFE (→transformers)
- Robust final optics and chamber transport: Focusing magnets for ion beams avoid direct line-of-sight damage from target debris/n-Y-radiation, and could last many full-power-years.
- Thick-liquid-protected chambers: Offer >30-year lifetime, no blanket changeout, potential near-surface-disposal of waste, and may avoid the need for a 14-MeV-neutron materials development program
- Unique target dynamics: Heavy ions stop by dE/dx with near-classical deposition (lasers stop at critical density and can undergo parametric instabilities). Ion range can be tailored by control of beam kinetic energy, ion species and target materials (→single-sided drive targets?)

Why heavy-ion drivers for inertial fusion energy?



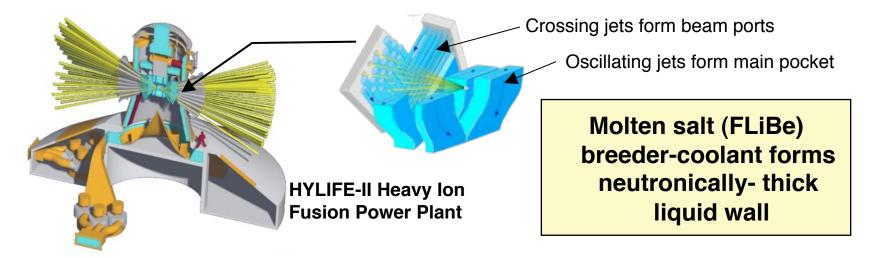


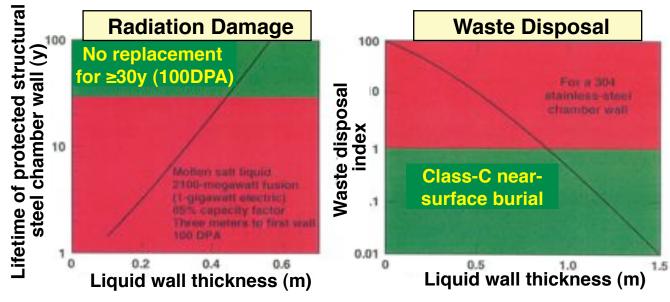
instabilities). Ion range can be tailored by control of beam kinetic energy,

ion species and target materials (→single-sided drive)

Heavy-ion power plant design: Thick liquid walls obviate 14MeVneutron material damage and need for blanket changeout

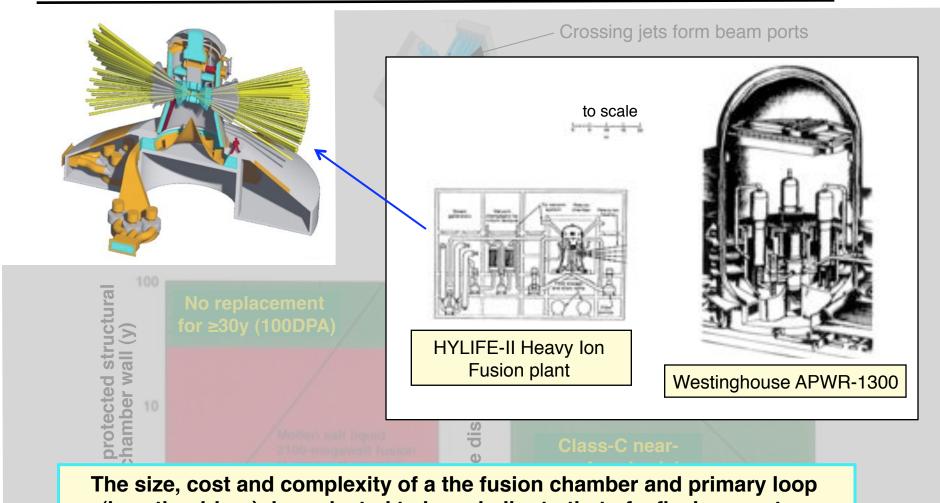






Heavy-ion power plant design: Thick liquid walls obviate 14MeVneutron material damage and need for blanket changeout





The size, cost and complexity of a the fusion chamber and primary loop (less the driver) is projected to be ~similar to that of a fission reactor.

The heavy ion driver is the single largest cost item in the plant

Liquid wall thickness (III)

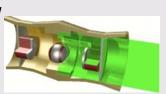
Liquia waii thickness (m)

Why **heavy** ions?



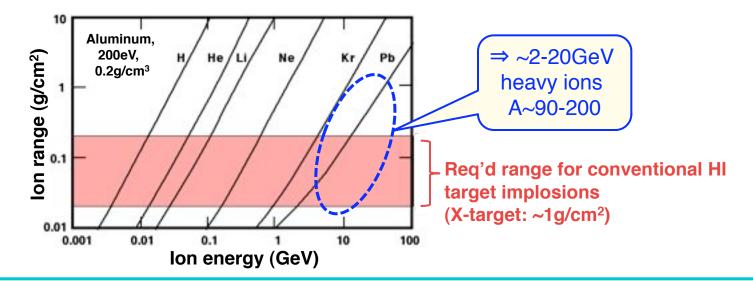
Target physics requires:

- Energy/power: ~2 6MJ drive energy delivered in ~ 10 ns, →~500TW
- Ion deposition range: ~ 0.02 0.2g/cm² (~1g/cm² for X-target)
- Focal spot dia: ~4-8mm



Deliver energy at higher ion kinetic energy:

- ⇒ lower beam current ⇒less space charge at focus
- ⇒ need higher ion mass to meet range stopping requirement



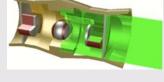
Heavy ion stopping in dense target plasmas is near-classical and predictable

Why **heavy** ions?



Target physics requires:

- Energy/power: ~2 6MJ drive energy delivered in ~ 10 ns, →~500TW.
- Ion deposition range: ~ 0.02 0.2g/cm² (~1g/cm² for X-target)
- Focal spot dia: ~4-8mm



These target requirements dictate the design requirements for the heavy-ion driver:

- short pulse lengths (~10ns)
- high peak powers (~100s TW)
- small focal spots (~5mm)
- at large focal distances (~5m)

This is manageable using heavy ions at high kinetic energies





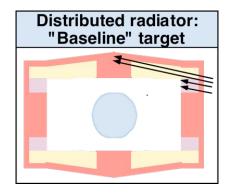
Heavy Ion Targets: There are several target classes under study....

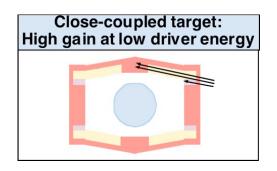
	Features	Issues
Indirect drive	Integrated 2D designs existAblation physics on NIFNatural two-sided geometry	 Low drive efficiency Lower gains, high driver energies
Direct drive X-target F.I	 Inherent one-sided drive, all-DT High coupling efficiencies Reduced stability issues Potential for high yields (~GJ) and gains 	 High gains require high densities under quasi-3D compression Higher ion kinetic energies High power hollow beams needed for fast ignition Driver concepts immature
Direct drive - tamped, shock ign. Single beam K.E ~3GeV Au tamper All-DT fuel/ablator DT gas	 High coupling efficiencies (tamped ablation) Simple targets High gains consistent with single ion-kinetic-energies (~2-10GeV) 	 Optimum ion species and energy Two-sided (polar) geometry to be established** Stability to be confirmed
(Dual density geometry) High ρ Low ρ	 Highest potential gains Potential one-sided drive Application to advanced energy conversion 	Complex hydro design process to achieve two-sided assembly

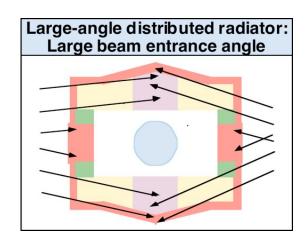
An integrated target-driver R&D program can be identified for each of these target design classes.

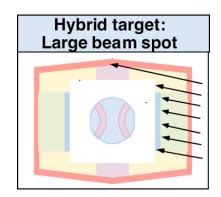
Indirect drive hohlraums with ~NIF hot-spot-ignition implosion physics: The U.S. has looked at a range of options

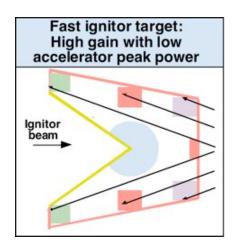


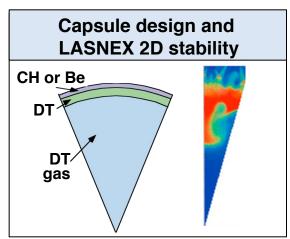








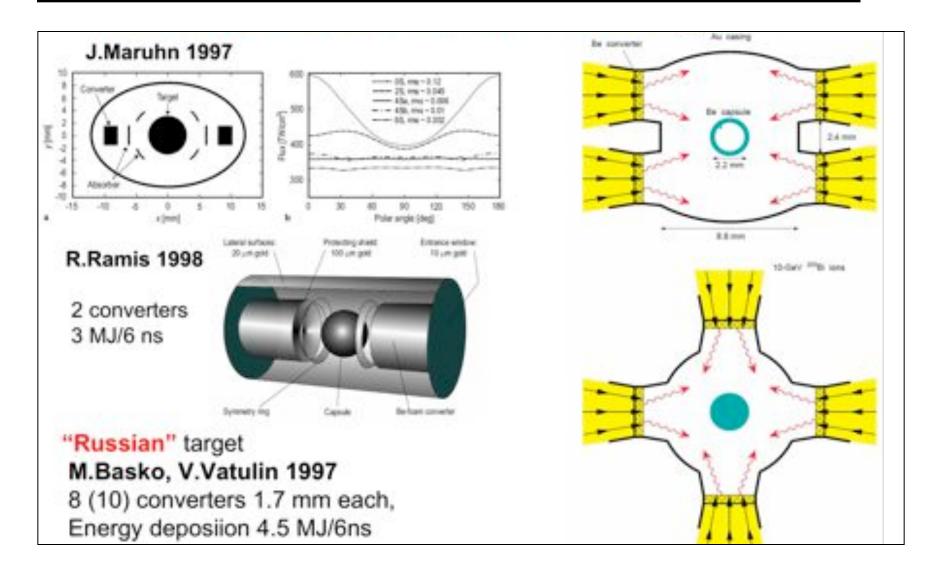




The capsule implosion physics for indirect drive heavy ion fusion will likely be validated on NIF

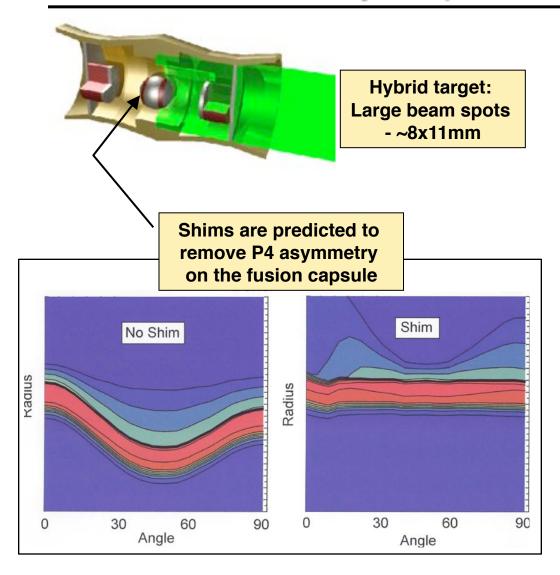
Indirect drive hohlraums with ~NIF hot-spot-ignition implosion physics: The Europeans have also been active in this area

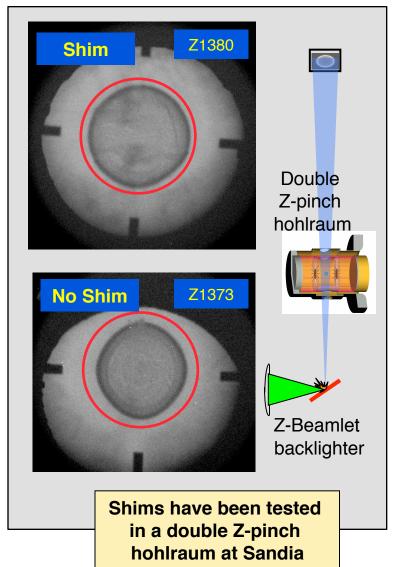




The U.S. hybrid target uses hohlraum shims for symmetric radiation flow - Shims are a relatively unexplored target optimization feature

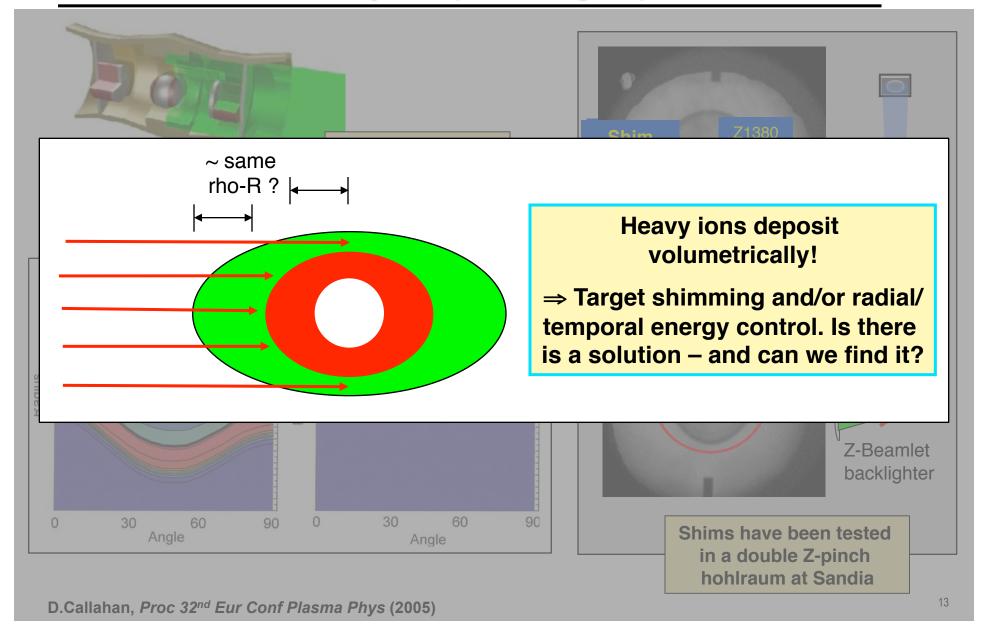






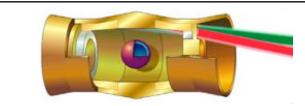
The U.S. hybrid target uses hohlraum shims for symmetric radiation flow – Shims are a relatively unexplored target optimization feature





Indirect drive hohlraums with ~NIF hot-spot-ign implosion physics: Three U.S. designs have been followed in detail





Standard Hohlraum

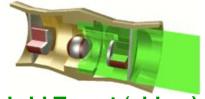
Gain ~60 at 6-7MJ (CCR=2.1 Beam spot ~3.5x8mm)



Close-Coupled

Gain ~130 at 3.3MJ

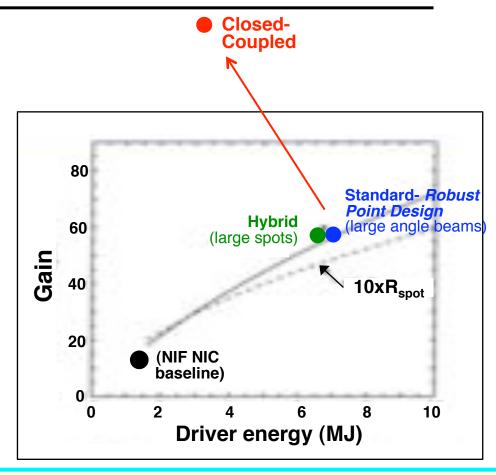
(CCR=1.6 Beam spot ~3mm)



Hybrid Target (shims)

Gain ~60 at 7MJ

(Beam spot ~8x11mm)



Heavy ion indirect drive will likely require larger driver energies

(but HI driver cost scales only as ~energy^{0.5})

The key to higher gain *Part-1*: Low implosion velocity



High target gain requires:

- Low V , ⇒ more fuel mass assembled for given driver energy

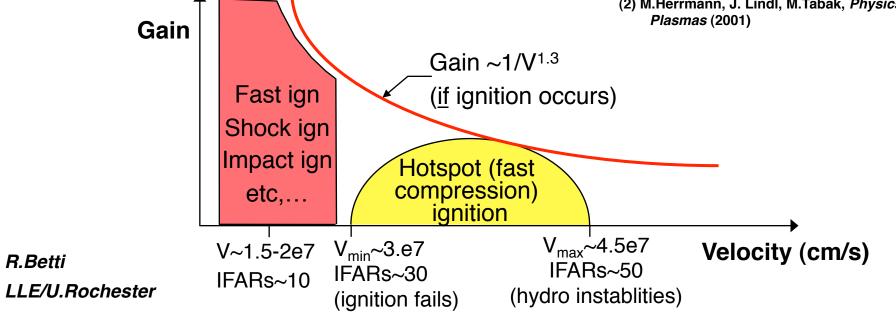
• High
$$\rho R$$
, \Rightarrow more fuel burnup $G = \frac{Y_{fusion}}{E_{driver}} = \frac{Y_{fusion}}{\frac{1}{2} m_{fuel} V^2 / \eta} \sim \frac{\rho R / (\rho R + 7)}{V^{1.3}}$

Ref. 1

But "hotspot" (= fast-compression) ignition needs high velocity to minimize ignition energy

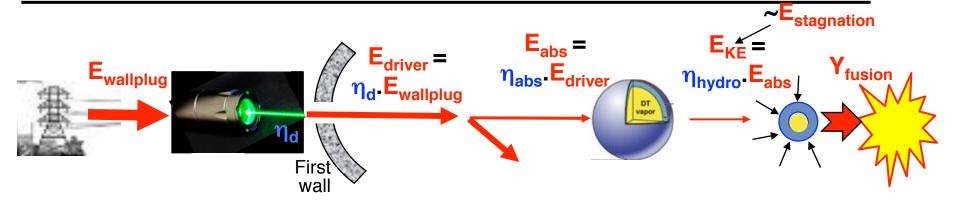
$$E_{ign-req'd} \sim rac{lpha_{FD}^{1.8}}{V^6}$$
 Ref. 2

- (1) R.Betti, C.Zhou, Physics Plasmas (2005)
- (2) M.Herrmann, J. Lindl, M.Tabak, Physics **Plasmas** (2001)



The key to higher gain *Part-2*: High driver-target coupling efficiencies



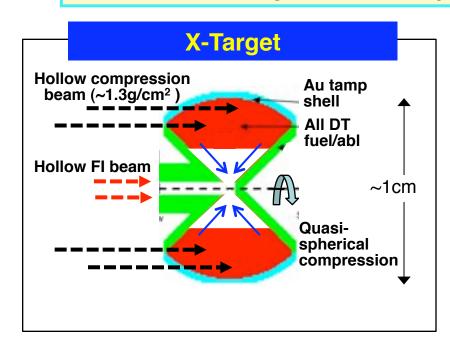


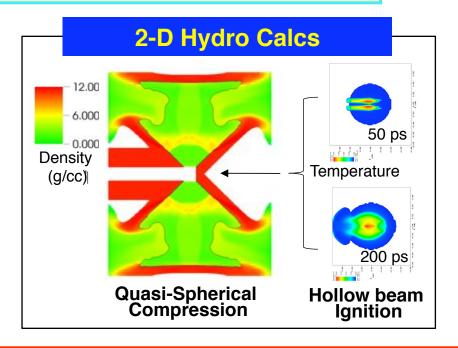
	Driver electrical efficiency η _d	Absorption efficiency η _{abs}	Hydro (rocket) efficiency η _{hydro}	System drive efficiency E _{wallplug} → E _{KE} = η _d · η _{abs} · η _{hydro}
Laser direct	~0.05-0.20	~0.85	~0.06-0.1 (ablative)	~0.01
Laser indirect	~0.05-0.20	~0.15-0.3	~0.1-0.15 (ablative)	~0.005
Heavy ion direct	~0.25-0.40	~0.9	~0.20 (tamped ablative)	~0.05
Pulsed power direct	~0.3		0.3 (direct agnetic)	~0.05

The heavy ion X-target: Potential for one-sided drive and high gain/yield



- Potential one-sided drive → thick liquid wall chambers
- Large fuel masses, all-DT, potential for high gains/yields ≥1GJ
- Low-velocity low-aspect-ratio fuel assembly
- More robust to high-mode stability low CR~7-10 (needs fast ignition)

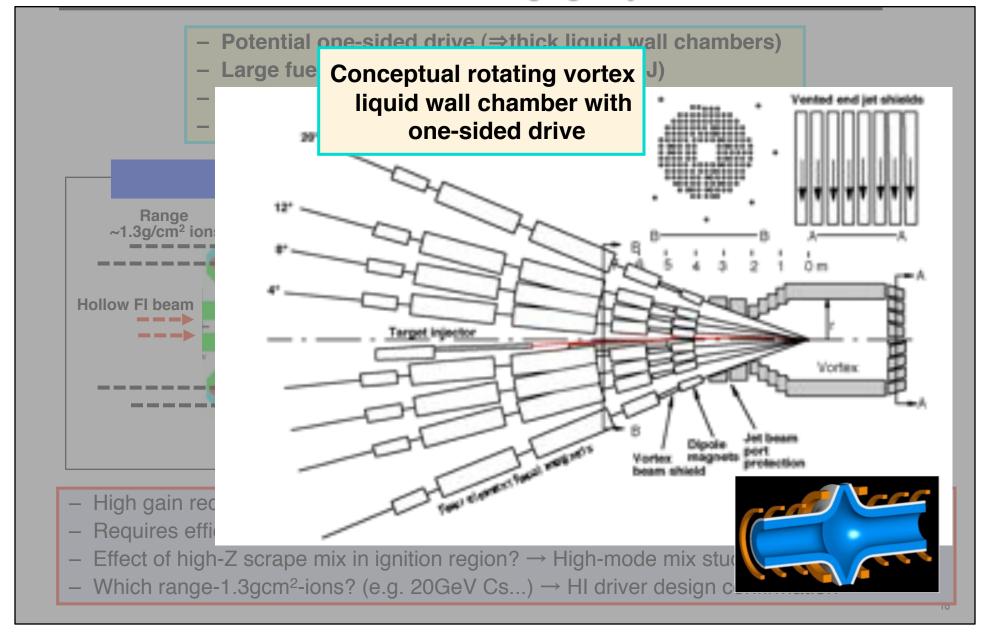




- High gain needs med-high-density quasi-spherical assembly → 2D hydro optimization
- Requires efficient ignition source \rightarrow *Hollow-beam fast ignition design (and B*_{θ} *lens?)*
- Effect of high-Z scrape mix in ignition region? → 2D-3D high-mode mix studies
- Driver design yet to be established →Need long ion ranges ~1.3g/cm² (20GeV Cs...?)

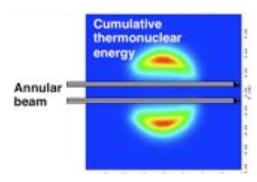
The heavy ion X-target: Potential for one-sided drive and high gain/yield



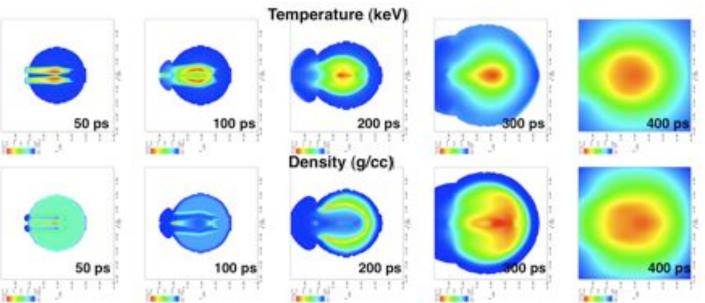


The heavy ion X-target: Simulation of fuel ignition and fusion burn using a hollow heavy-ion fast ignition beam





- Previous 2D studies of hollow-beam ignition in compressed fuel have been performed by Herrmann, Tabak and Artzeni
- Here: Initial compressed fuel: 800 μm sphere, 50 g/cm³.
- 60 GeV U hollow beam , 750 kJ, 50 ps, 200 μm dia.



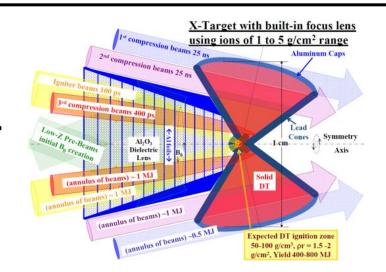
Fusion yield =750MJ

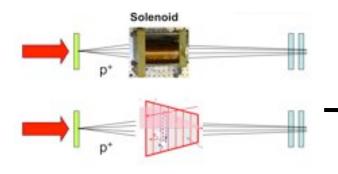
Stringent pointing, focusing and power requirements will require innovative beam physics solutions and attention to appropriate range ion species (20GeV Cs...?)

The X-target enhances 6-D phase space focusing potentially sufficient for fast ignition: But much design work to do!



Potential built-in magnetic B_{θ} focusing lens increases focusing angles permitting large initial spot sizes for fast ignitor beam (~1rad focus angles over ~1cm with large ~1g/cm² ion range)



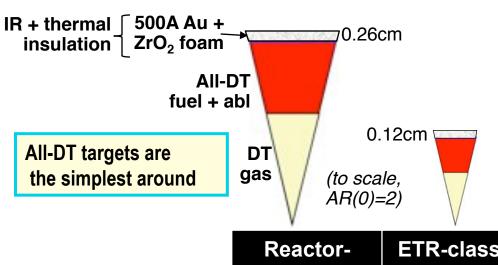


With new 100TW compressor, GSI (Darmstadt) will explore the laser driven magnetic lens in the near future

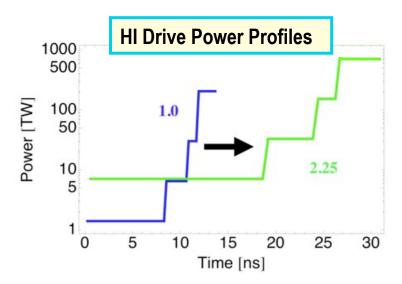
- High gain needs med-high-density quasi-spherical assembly \rightarrow 2D hydro optimization
- Requires efficient ignition source \rightarrow Hollow-beam fast ignition design and B_{θ} lens
- Effect of high-Z scrape mix in ignition region? → 2D-3D high-mode mix studies
- Which range-1.3gcm²-ions? (e.g. 20GeV Cs...) → HI driver design confirmation

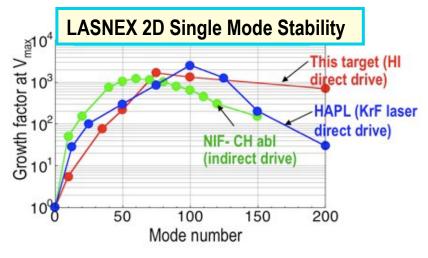
Heavy ion <u>direct</u> drive (untamped): Efficient drive but requires low kinetic energy beams in the foot pulse \rightarrow Focusing constraints?





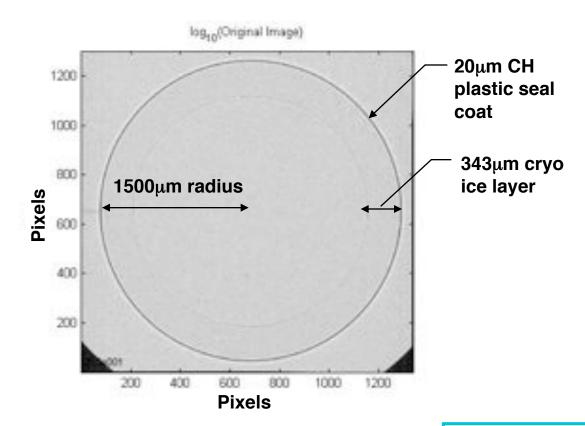
	Reactor- class	ETR-class, NIF-equiv.
Yield (MJ) / Gain	560 / 160	20.8 / 47
HI driver energy (MJ)	3.5	0.44
Ion kinetic energies foot/main (GeV)	0.22/2.2	0.05/0.5
Peak drive power (TW)	660	205
in-flight adiabat $lpha$	2.1	3.2
η _{abs} * η _{hydro}	0.08	0.09





All-DT direct drive targets are the simplest around. LLE(U.Roch.) have made analogous capsules with the required specifications



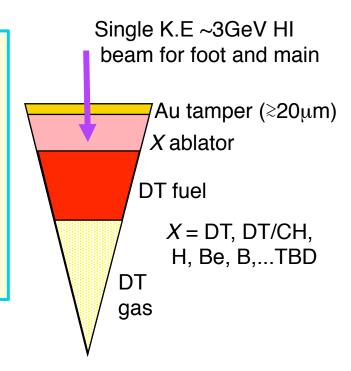


LLE cryo target
X-ray phase contrast image
(courtesy D.Harding LLE)

Direct drive: A solution to the low ion kinetic energies in the foot pulse may be found in tamped "cannonballs"



- Tamped cannonballs (TCs) can be driven with a single high-energy (~2-10GeV) ion species
- TCs have high hydro efficiency ≤20% (combination of direct and radiation) that compensates for energy loss in tamp
- Addition of shock ignition may enable gains ~100 at ≥1MJ
- Further gain increases in gain are possible with zooming



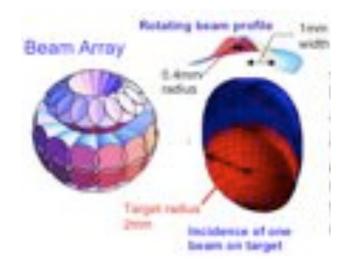
- Optimum ion species and kinetic energies TBD → Tradeoff between tamp thickness and drive efficiency
- Stability to be confirmed → Ion-driven instability (but low velocity, fat shells with high ablative ion-range/radiation smoothing)
- Two-sided polar drive geometry to be established → Will leverage NIF PPD optimization studies (but heavy-ions don't refract)

Direct drive: It is important to retain thick liquid wall options for heavy ion fusion \Rightarrow Two- sided polar direct drive?



We are leveraging current NIF studies that are optimizing polar drive symmetry through pointing, focusing and power control

350TW 175TW 175TW 95TW Composite drive Focused at r_{shock} Symmetry Focused at ro 48 quads. axis - 24 quads, 24 quads. - 192 beams - 96 beams 96 beams All-DT fuel and ablator. Lower set of aspect ratio 2.7; ~0.5MJ-drive, gain-60, 30MJ yield Symmetry control: 8 rings of (split) guads independently power phased; 16 rings of beams, top and bottom, all independently pointed and focused:



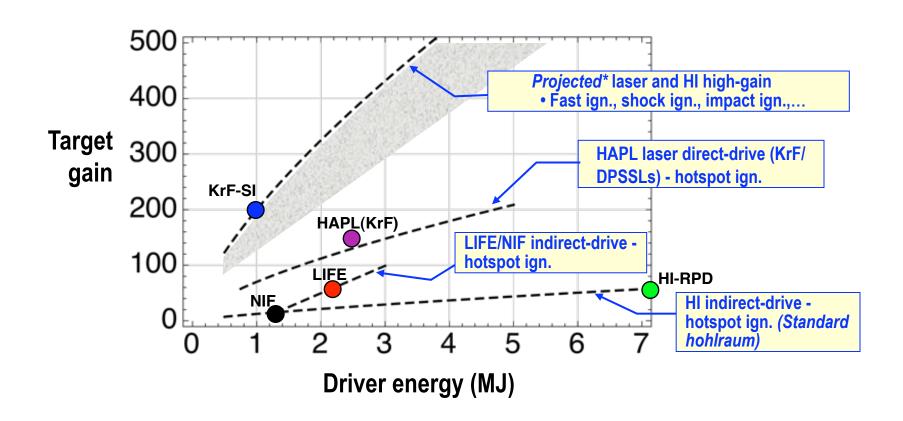
Four annular rings of HI beams (15 each, 60 total) with hollow rotating spot can give ~0.7% intensity variations

J. Runge *Phys.Plasmas* <u>16 (</u>2009)

NIF lower 24 quads (96 beams)



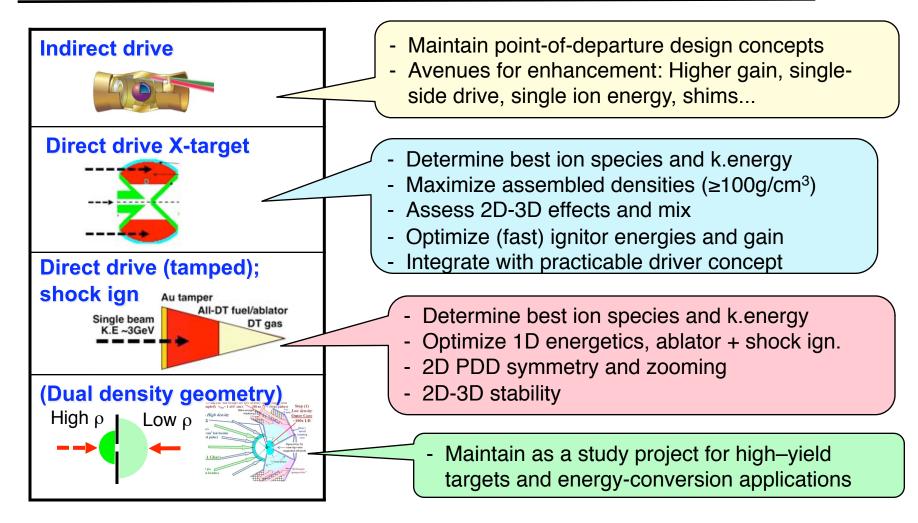




^{*} Projected = projected in 1-D and initial 2-D studies but not fully established in integrated designs

Where to from here: Modeling, simulation and experiments

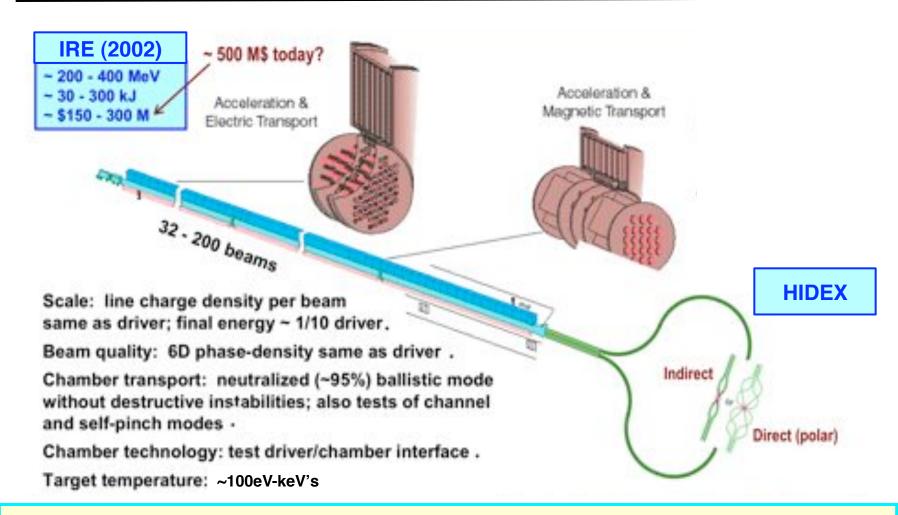




....with input from NIF and Omega experimental data iterated with HIDIX accelerator target design using models improved with NDCX-II data.

The Heavy Ion Driven Implosion Experiment (HIDIX) would enable target implosion experiments at 10's-100's kJ



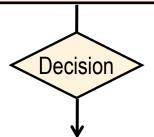


The Integrated Research Experiment (IRE) design from Snowmass-2002 could drive HIDIX for both direct and indirect drive targets

Heavy ion fusion development strategy: Target physics is integrated into the R&D phases to HIF-ETR/Demo

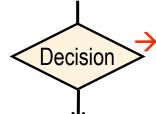


PHASE I: First 5 years: Integrated single beam accelerator experiments, benchmarked simulations, enabling technology development (e.g., magnet arrays), scaled liquid chamber experiments), target designs for several target options, systems analysis.



→ Deliverable: validation of selected heavy ion accelerator and target approach for Phase II & III

PHASE II: Next 10 years: Construct/operate 10-100kJ-scale Heavy-Ion-Driven Implosion Experiment (IRE-HIDIX), supporting liquid chamber, target design, target fabrication, injection R&D for 5 Hz burst-mode target experiments. Technology development for Phase III.



→ **Deliverable:** validation of integrated multiple-beam accelerator, chamber & target design for Phase III

PHASE III: Next 20 years: Construct 2-3 MJ HIF ignition test facility for single shot tests, then burst mode, using accelerator designed for 5 Hz. If successful, add nuclear systems to upgrade to 150 MW average-fusion-power level HIF-ETR/DEMO.











Backup slides

US IFE program: ~7 M\$/yr (constant 2010 \$) x 30 years~ \$200 M(constant 2010 \$) ~2 FTE/yr ave for 20years = ~10 M\$ (constant 2010) - ~4% of NIF/NIC target effort





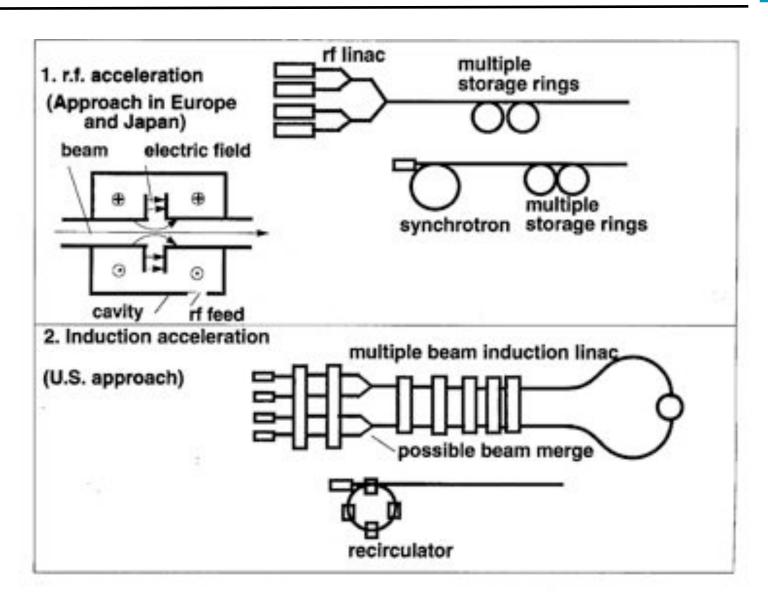






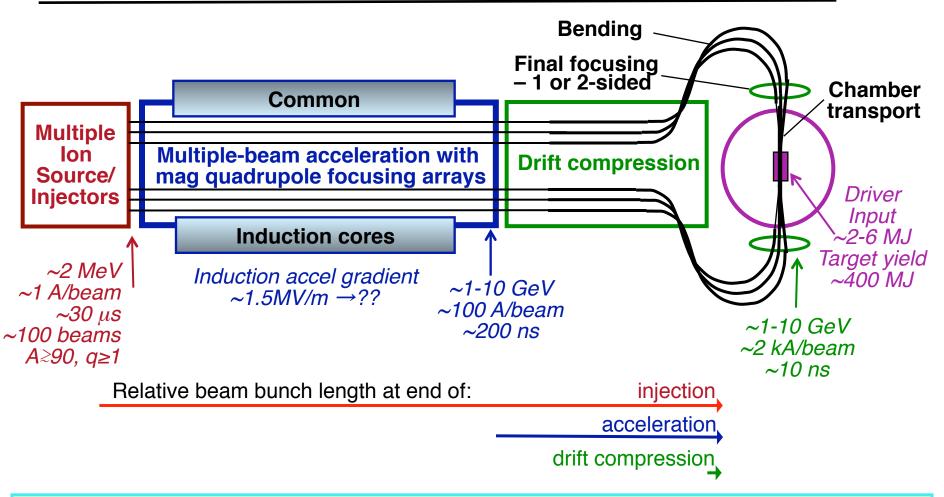
There are two principle methods of ion acceleration to GeV energies





We have established design baselines for multiple-beam quadrupole-focused induction linac drivers





Power amplification to required ~10TW per beam is achieved by acceleration and longitudinal bunching (drift compression) of mildly-relativistic ions

Significant scale up of accelerator energy and peak power @ relevant ion target range is needed for an HIF driver.

	NDCX-II	GSI-SIS18	LHC	HIF driver
Ion energy	1.2→ 6 MeV	70 GeV	14 TeV	10 GeV
	(Li+)	(U ²⁸⁺)	(p)	(Pb ⁺)
Beam power	0.1 to 1 GW	350 MW	1 TW	4 TW / beam
	(50Ax2MeV	(in 130 ns)	(100 μs dump)	X100 beams
	→150Ax6MeV)			(in 8.2 ns)
Beam energy	0.08 to 0.25 J	45 J	100 MJ	6 MJ
			(total dump)	
Space charge	High	Very Low	Negligible	High to low
$\Delta \phi$ /KE (final)	5 x 10 ⁻²	10 ⁻⁹		10 ⁻¹ to 10 ⁻⁵
Ion range	Low	High	Way too high	IFE target
	(~ 3 μm foil)	(> WDM target)	for IFE	requirement
	0.0001 g/cm ²	10 g/cm ²	10,000 g/cm ²	0.03 -1 g/cm ²









R&D roadmap to determine the feasibility of heavy ion fusion energy (#'s=M\$/yr)

Fiscal Year	2009	•	2013	2014		2018	2019	- 8	2023	2024	8	2028	2029	2033
Integrated single beam HEDP/IFE exps. to maximize pressure in planar targets	7 M	S/yr	→ 15	25	→	20	20	>	20	15	→	15	est to the stay of	
NDCX-I (to 10 kBar)	7(@1	bt:	1 (a PPP	L) -	5							Optim	ize plasma
NDCX-H(1) (to 1 MBar)			12 -	→ 13								-	Drift.	bend & focus
NDCX-II+→IB-HEDPX(1) (to 10 MBar)			1	10	/	13 -	→ 11	->	6				Upgr	ade to 8 MV
Intl. Collab. Exps. @ FAIR, LANSCE			1		->	2 -) 4		→9			→ 10	High I	CE ions
(each row includes theory/sim and equipment	suppe	ort)	- 4	<5-y1	Pha	se I >	Key d	fecisio	on (CD	2 for	HIDI	X)		
Accelerator driver R&D for 5 Hz, multiple-beam target experiments	0.6	>	2.5	11	>	14	25	>	100	100	>	90		→90
5 Hz accelerator R&D (inc. HCX-II)(2)			1.5	8		8	15	->	15	15				HI HI
Exp. target R&D (design/fab/inj.)	0.3	>	0.5	1		2	2.5							
Long-path accelerator R&D(UMER,PT)	0.3	->	0.5	2	>	2 \	/ 2.5							
Heavy Ion Driven Implosion Experiment (HIDIX) (5Hz, 100 MBar)	1500					2 -	5	80	x 6 yr			80		
									K	ey De	cision	(CD2	or H	IFTF)
Heavy Ion Fusion Nuclear Science and Technology ⁽³⁾	0.4		1.5 -	→ 3		→5→	20		→ 30	→40		→ 75		→310?
5Hz HIF target design, fab, inj., tracking	0.3	->	1	2	->	2.5	10	->	15	20		→ 30		
Enabling liquid chamber R&D	0.1		0.5 -	→ 1	>	2.5	10	\rightarrow	15	20		→ 30		
Heavy Ion Fusion Test Facility (HIFTF) -100 MJ yield single shot and 5 Hz											10	→ 15		250 x 8 yr ? -
Fiscal Year	2009		2013	2014		2018	2019	7	2023	202	4	2028	2029	2033
(All costs in M S per year) Total HIF(1)	8	>	19	38	>	40	65	→	150	155	3	180		400?

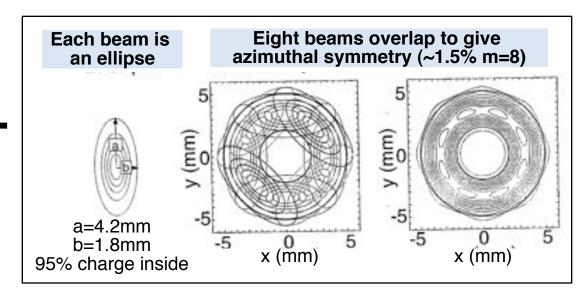
(1) Budgets include HEDLP relevant to HIF, but not operations & diagnostic support for grant-funded HEDLP users
(2) Includes multiple beam injectors, transport, and final focus arrays needed for HIDIX
(3) Does not include MFE nuclear science and technology that may be applicable to HIF

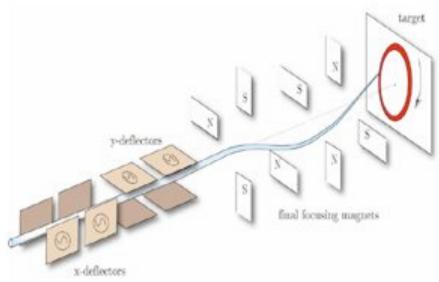
Design Construction Operation/R&D

A deflecting wobbler field may be an effective technique for beam smoothing, uniform deposition and instability suppression



Conventional design uses multiple overlapping beams with static focil





Application of wobbler field is being investigated for producing annular hollow beams together with potential beam smoothing and R-T stabilization

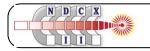
Conjecture

"If a big accelerator lab had made a commitment to develop heavy ion fusion in 1975, as LLNL did for laser fusion, and had spent the same amount of money as was spent on either (a) laser fusion (~200M/yr x 30 years= ~6B\$) or (b) high energy particle accelerators for science (~400 M x 30 yr=12 B\$), it is virtually certain that a 5-10 MJ heavy ion accelerator would be available today for ignition studies.

The accelerator would have evolved differently, towards ~3-10 GeV instead of ≥1TeV(to stop the beams in targets), and towards 50-100 parallel beams, instead of 1 beam (for illumination symmetry)."

B.G. Logan,

Director, Heavy Ion Fusion Science Virtual National Laboratory, February 12, 2011.



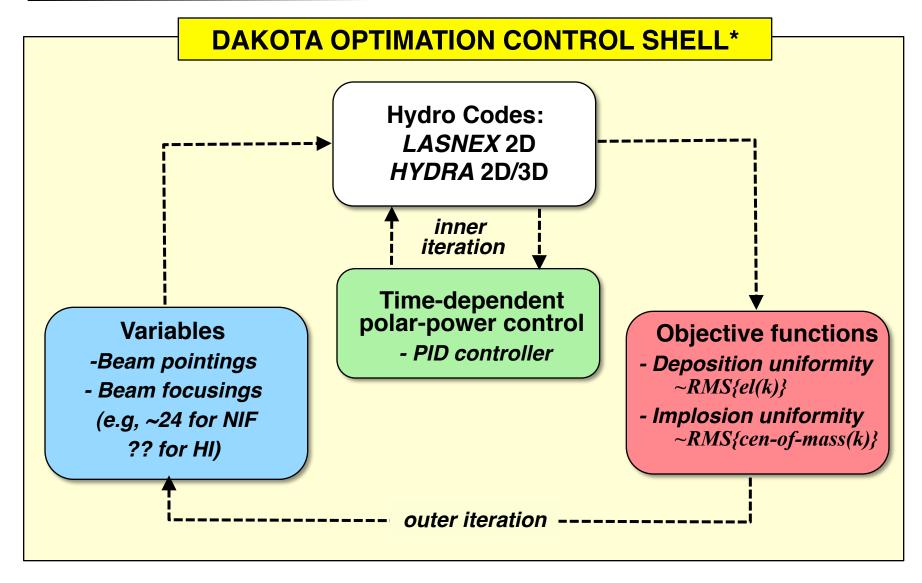






Heavy Ion Polar Direct Drive: Our optimization formalism will exercise LLNL computation facilities to their limit



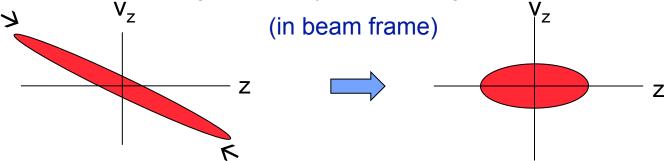


^{*} DAKOTA – Sandia National Laboratory, http://www.cs.sandia.gov/DAKOTA/index.html (= "UQ Pipeline" at LLNL)

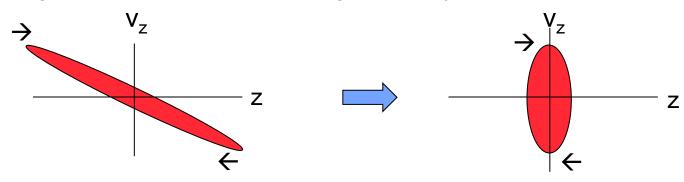
Drift compression is used to longitudinally compress an ion bunch



- Induction cells impart a head-to-tail velocity gradient ("tilt") to the beam
- The beam shortens as it "drifts" down the beam line
- In **non-neutral drift compression**, the space charge force opposes ("stagnates") the inward flow, leading to a nearly mono-energetic compressed pulse:



• In **neutralized drift compression**, the space charge force is eliminated, resulting in a shorter pulse but a larger velocity spread:



Heavy Ion Fusion beam physics experimental/modeling status



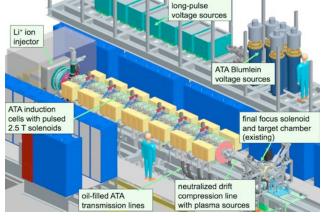
- Experiments and simulations have addressed most driver beam manipulations, giving confidence to projections of beam brightness on target.



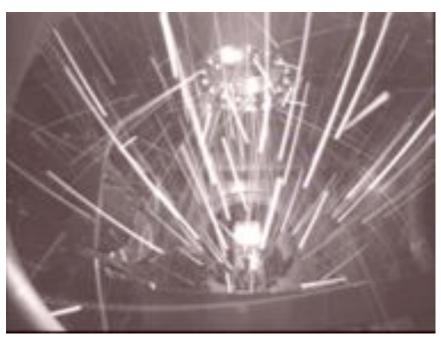


- The Neutralized Drift Compression Experiment-II (NDCX-II) at LBNL should reach ~100A on target →
- Studies of heavy ion power plants predict a COE similar to that of other fusion options, assuming that:
 - it'll be possible to fabricate targets inexpensively
 - liquid-wall target chambers can be cleared rapidly
 - cost-effective drivers can be built.

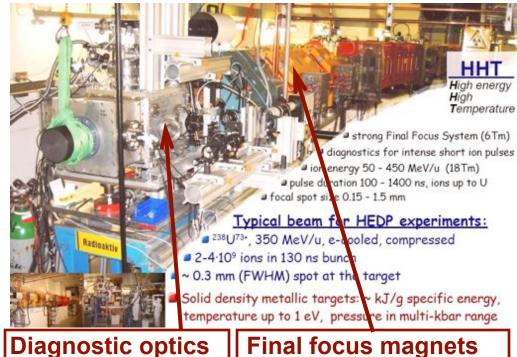




VNL targets have been heated with 0.3 A, 83 GeV U⁺⁷³ ions focused to 150μm radius spots on target at GSI Darmstadt



Visible ms camera frame showing hot target debris droplets flying from a VNL gold target (~ few mg mass) isochorically heated by a 130 ns, 50 J heavy ion beam to ~ 1 TW/cm² peak and 1 eV in joint experiments at GSI, Germany.



The new FAIR upgrade of GSI's accelerator will allow joint cryo hydrogen compression experiments relevant to heavy ion fusion with much more (80 kJ) of uranium beam energy.











Ion stopping in HYDRA and LASNEX rad-hydro target codes



$$-\frac{dE}{dx} = \left[\frac{4\pi e^4}{m_e c^2}\right] \left[\frac{N_q \rho_T}{A_T}\right] \left[\frac{Z_{eff}^2}{\beta^2}\right] \left\{(Z_T - \overline{Z}) \log \Lambda_g + \overline{Z} G(\beta / \beta_e) \log \Lambda_f\right\}$$

$$= \sum_{S: r-22 \text{ leV cm}^2} \frac{m_{S, r}}{m_e c^2} \left[\frac{N_q \rho_T}{A_T}\right] \left[\frac{Z_{eff}^2}{\beta^2}\right] \left\{(Z_T - \overline{Z}) \log \Lambda_g + \overline{Z} G(\beta / \beta_e) \log \Lambda_f\right\}$$

 $\rho_T = \text{target density in } g / cm^3$, $A_T = \text{target atomic weight}$

 Z_T = target atomic number, \overline{Z} = target ionization state

$$\Lambda_{\theta} = \frac{2m_sc^2\beta^2}{\tilde{I}}$$
, $\Lambda_{\theta} = \frac{m_sc^2\beta^2}{\hbar\omega_s}$, $G(x) = erf(x) - x erf'(x) = 1$ for $x >> 1$.

 \bar{I} = average ionization potential = .01 Z_T keV (Bloch's rule)

$$\omega_p = \text{plasma frequency} = \sqrt{4\pi e^2 n_p / m_p} = 56416 \sqrt{n_p / \text{sec}}$$

$$\hbar\omega_p = (3.7e-14)\sqrt{n_e} \text{ keV}$$
, $n_e = \text{electron density in } 1/\text{cm}^2 = \overline{Z}N_0\rho_T/A_T$

Ion Beam :
$$\beta = w/c$$
, $\gamma = \frac{1}{\sqrt{1-\beta^3}} = 1 + \frac{E}{Mc^3}$

E =Kinetic Energy of Ion Beam in keV.

 Mc^2 = Ion Beam Rest Energy = $A_{instrue}$ (9.3e5) keV

 $m_e c^2$ = Electron Rest Energy = 511 keV

Betz Empirical
$$Z_{eff} = Z_{toolean} \left[1 - \exp(-137 \beta_{eff} / Z_{toolean}^{AS}) \right]$$

$$\beta_{sf}^{2} = \beta^{2} + \beta_{s}^{2}$$
, with $\gamma_{s} = \frac{1}{\sqrt{1 - \beta_{s}^{2}}} = 1 + \frac{kT_{r}}{m_{s}c^{2}}$

Relativist is Correction: Log $\Lambda_s \rightarrow \text{Log } \Lambda_s + R$, Log $\Lambda_r \rightarrow \text{Log } \Lambda_r + R/2$ where $R = 2 \text{ Log } \gamma - \beta^2$